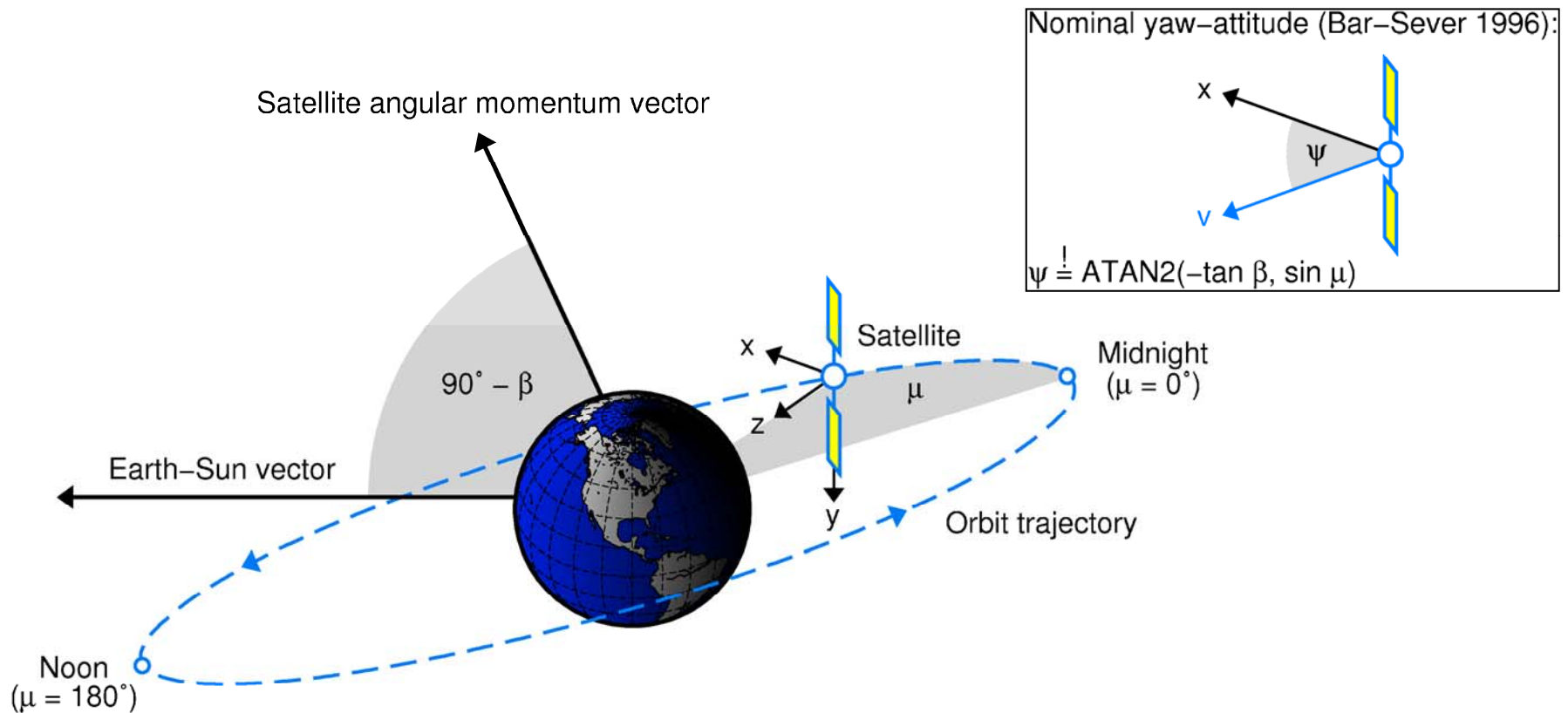


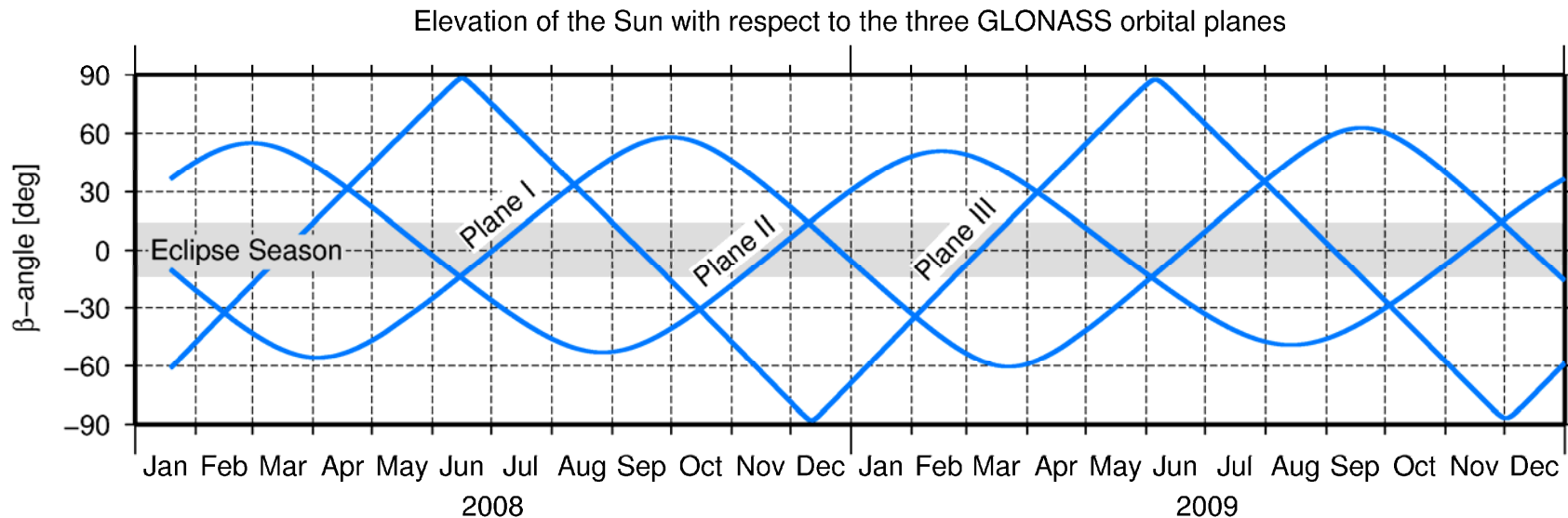
# Modelling the GLONASS-M satellite yaw-attitude during eclipse seasons

F. Dilssner, T. Springer, J. Dow  
IGS Workshop, Newcastle, England  
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# Attitude constraint: Sun-Earth-pointing

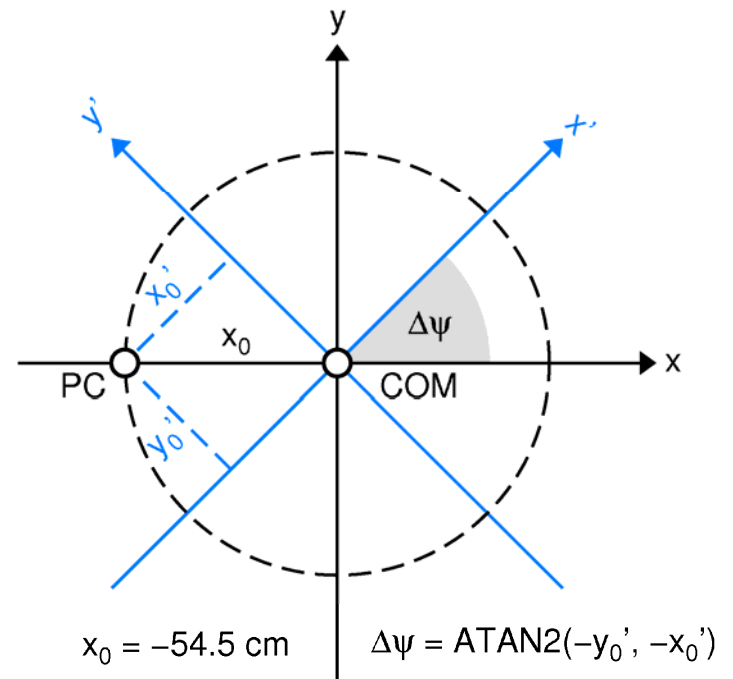


$\beta$  = elevation of the Sun with respect to orbital plane;  $\mu$  = geocentric orbital angle between satellite and midnight

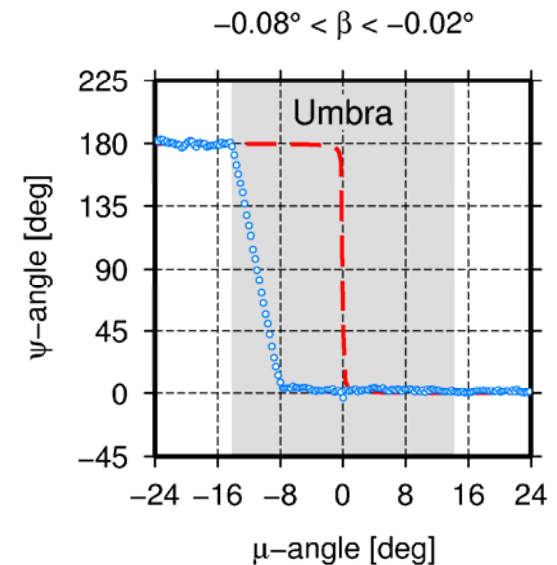
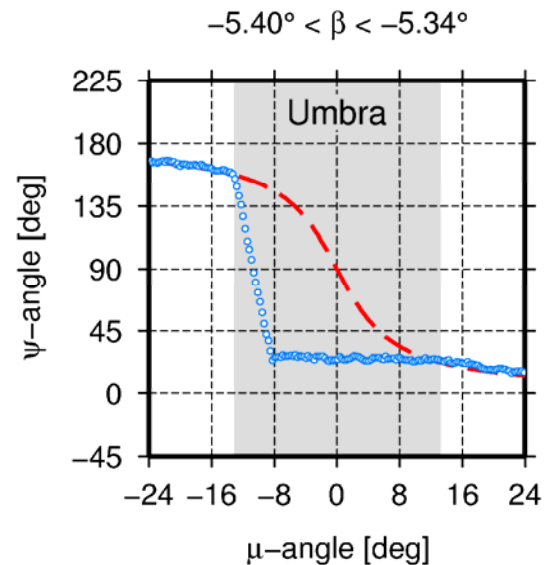
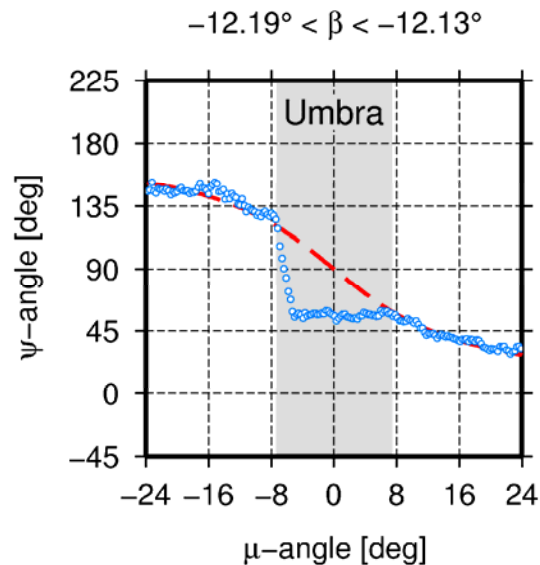


- $\beta$ -angle varies while the Earth revolves around the Sun
- Modelling of yaw-motion challenging during eclipse season ( $|\beta| < 14.2^\circ$ )
- Solar sensors can no longer control attitude due to absence of sunlight
- GLONASS-M attitude control in Earth's shadow? Noon-turn manoeuvre?

- Lack of telemetry data
- 30-second code & phase measurements from global GPS/GLONASS network
- 1<sup>st</sup> step: IGS-like multi-GNSS analysis
- 2<sup>nd</sup> step: Estimation of satellite clocks & phase centre positions epoch-by-epoch (“reverse kinematic point positioning”)
- Nominal yaw-attitude model employed
- Yaw error reflected in horizontal PCOs

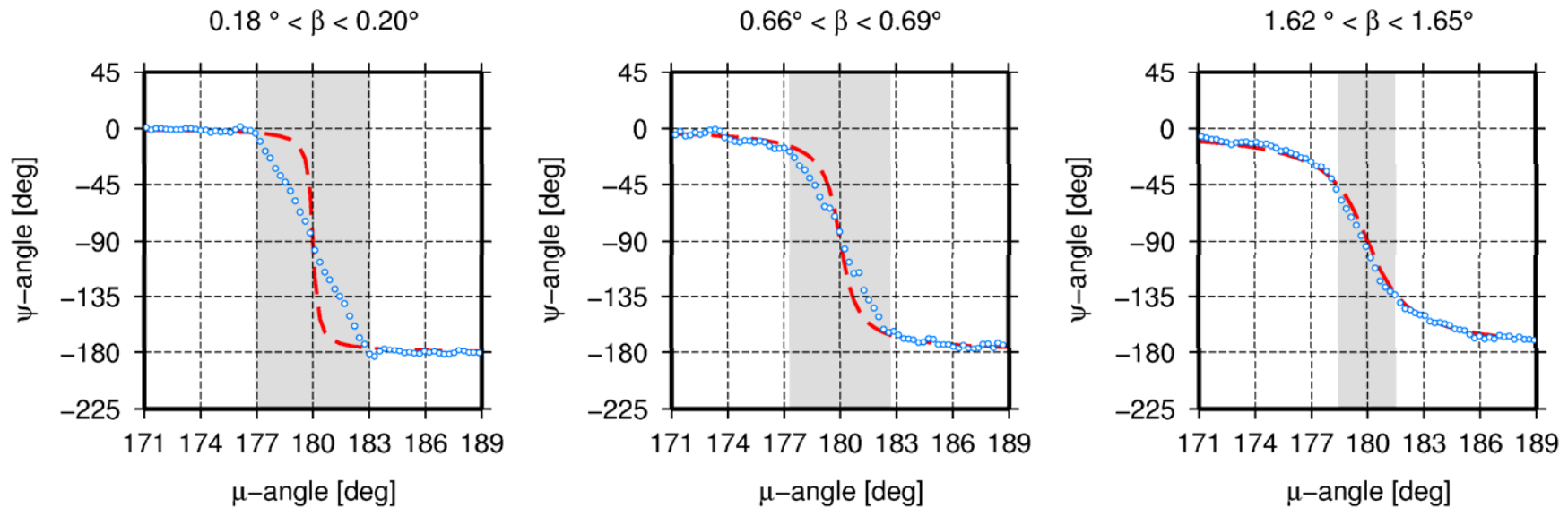


# Shadow-crossing manoeuvre



- Linear drift in estimated yaw-angle as soon as s/c enters umbra
- S/c is spinning around its z-axis with maximum rate ( $R \approx 0.25^\circ/s$ )
- Sense of rotation is equivalent to nominal rotation direction
- S/c switches into fixed-yaw mode at the end of required midnight-turn

# Noon-turn manoeuvre



- S/c is spinning its z-axis with maximum rate ( $R \approx 0.25^\circ/\text{s}$ )
- Maximum duration 12 min; maximum yaw error  $\pm 90^\circ$
- Required yaw rate around noon exceeds hardware rate  $R$ , if  $|\beta| < 2.0^\circ$
- Manoeuvre already starts before required yaw rate exceeds  $R$  ( $\neq$  GPS)

# The new GLONASS-M yaw-attitude model



- Shadow-crossing regime:

$$\psi(\mu) = \begin{cases} \text{ATAN2}(-\tan \beta, \sin \mu_s) + \frac{\text{SIGN}[R, \dot{\psi}(\mu_s)] \cdot (\mu - \mu_s)}{\dot{\mu}} & \text{if } \mu_s < \mu < \mu_f \\ \text{ATAN2}(-\tan \beta, \sin \mu_e) & \text{if } \mu_f < \mu < \mu_e \end{cases}$$

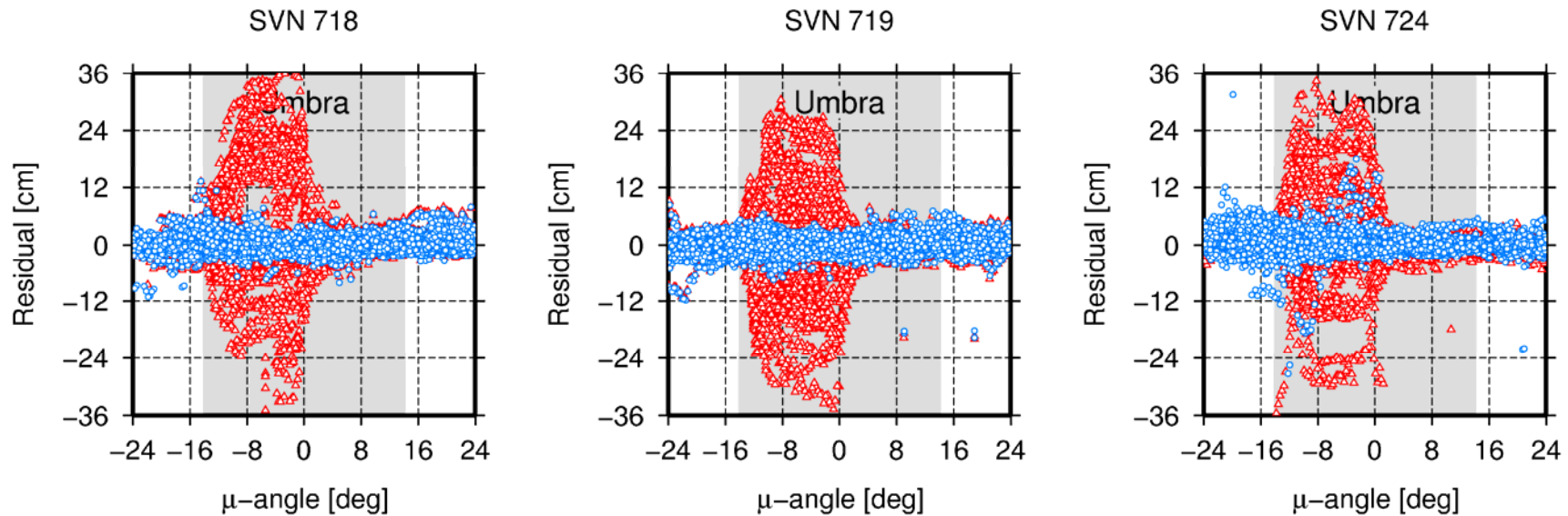
$$\mu_f = \frac{\dot{\mu} \cdot [\text{ATAN2}(-\tan \beta, \sin \mu_e) - \text{ATAN2}(-\tan \beta, \sin \mu_s)]}{\text{SIGN}[R, \dot{\psi}(\mu_s)]} + \mu_s, \quad \mu_e = -\mu_s = \arccos(\cos \beta_0 / \cos \beta)$$

- Noon-turn regime:

$$\psi(\mu) = \text{ATAN2}(-\tan \beta, \sin \mu_s) + \frac{\text{SIGN}[R, \dot{\psi}(\mu_s)] \cdot (\mu - \mu_s)}{\dot{\mu}} \quad \text{if } \mu_s < \mu < \mu_e$$

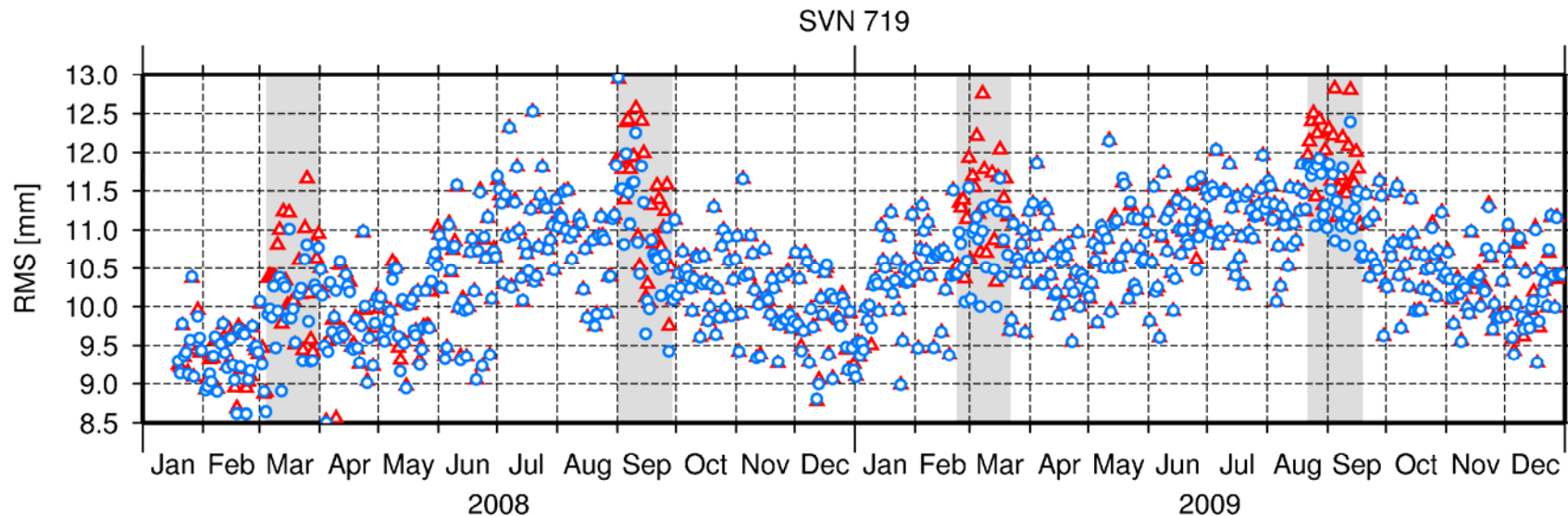
$$\mu_s = \frac{\arctan(|\beta| / \sin \mu_0) + |\beta| \mu_0 \cos \mu_0 / (\beta^2 + \sin^2 \mu_0) + \pi R / \dot{\mu} - \pi / 2}{R / \dot{\mu} + |\beta| \cos \mu_0 / (\beta^2 + \sin^2 \mu_0)}, \quad \mu_e = 2\pi - \mu_s$$

# Carrier phase residuals



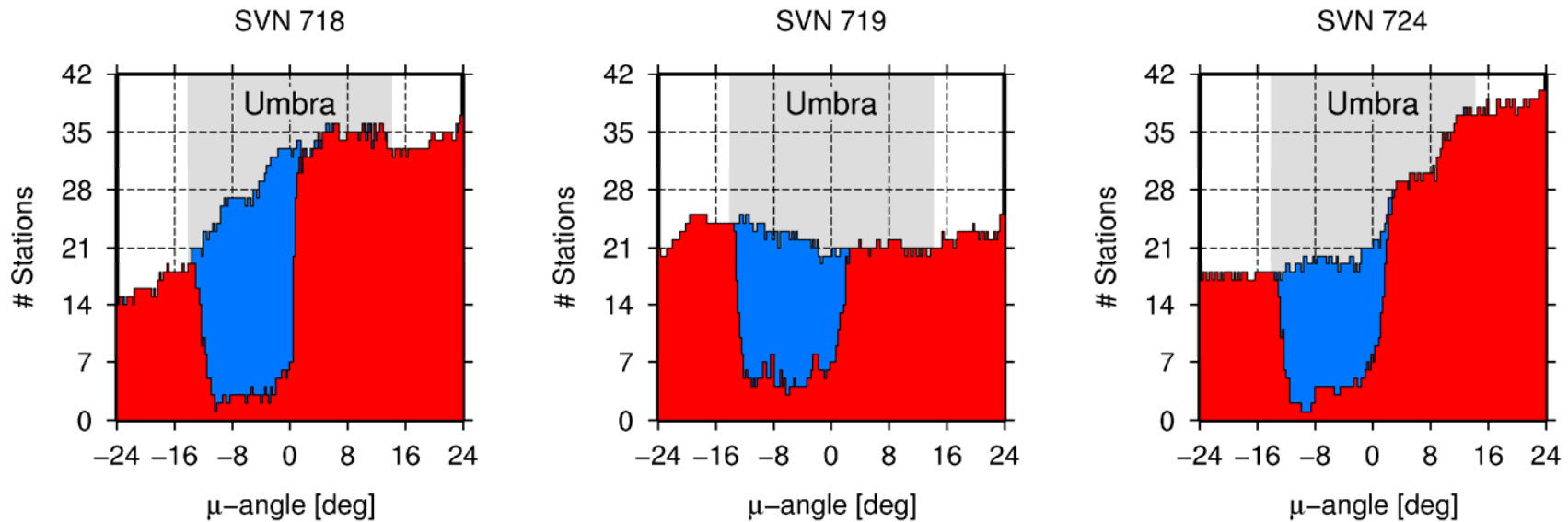
- Reprocessing of 30-second satellite clock solutions w/o solving for PCOs
- Nominal attitude model (*red*) vs. new attitude model (*blue*)
- Range error due to mismodelling of satellite APC correction during noon and midnight may amount to  $\pm 19$  cm and  $\pm 27$  cm, respectively

# Daily carrier phase RMS

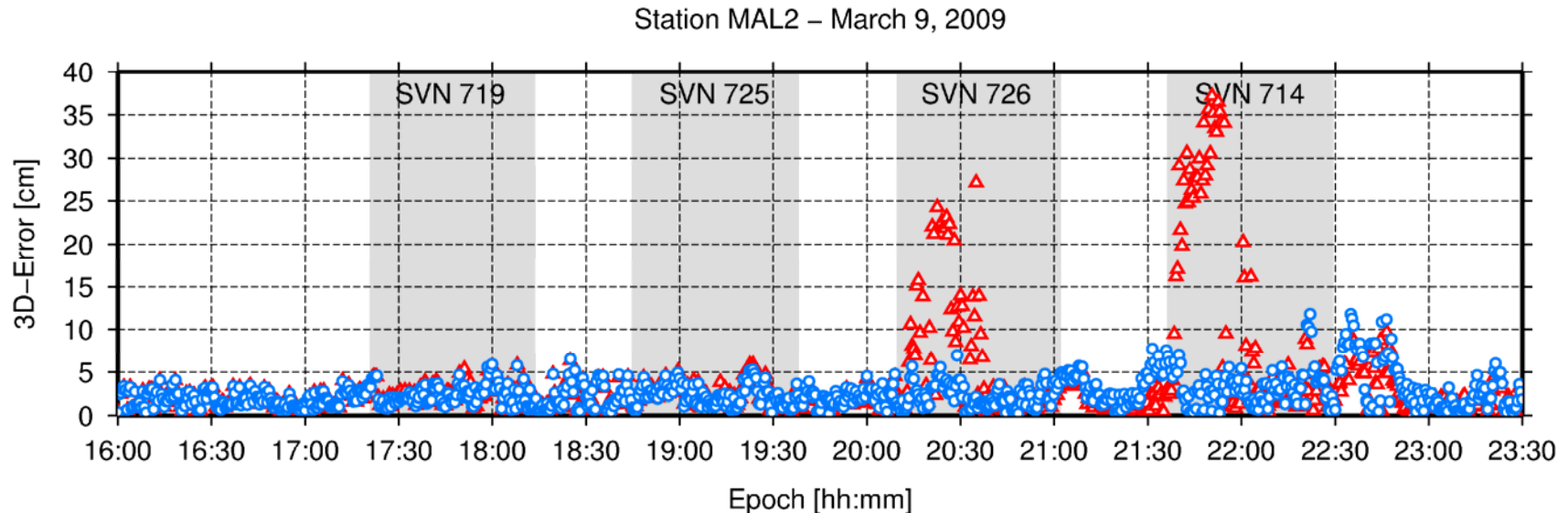


- Nominal attitude model (*red*) vs. new attitude model (*blue*)
- RMS values during eclipse seasons  $\sim 10\%$  higher (*red*)
- Reduction to "normal" level when employing new attitude model
- Improvement goes along with increased number of observations ( $\sim 2.5\%$ )

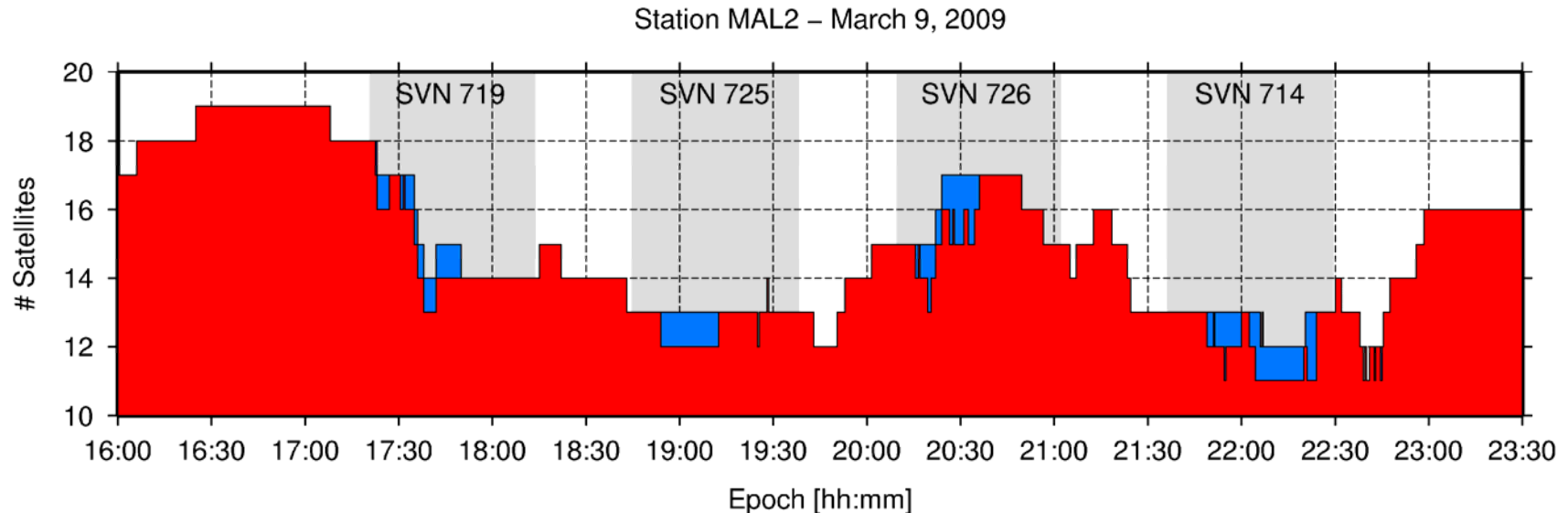
# Observability of satellite clocks



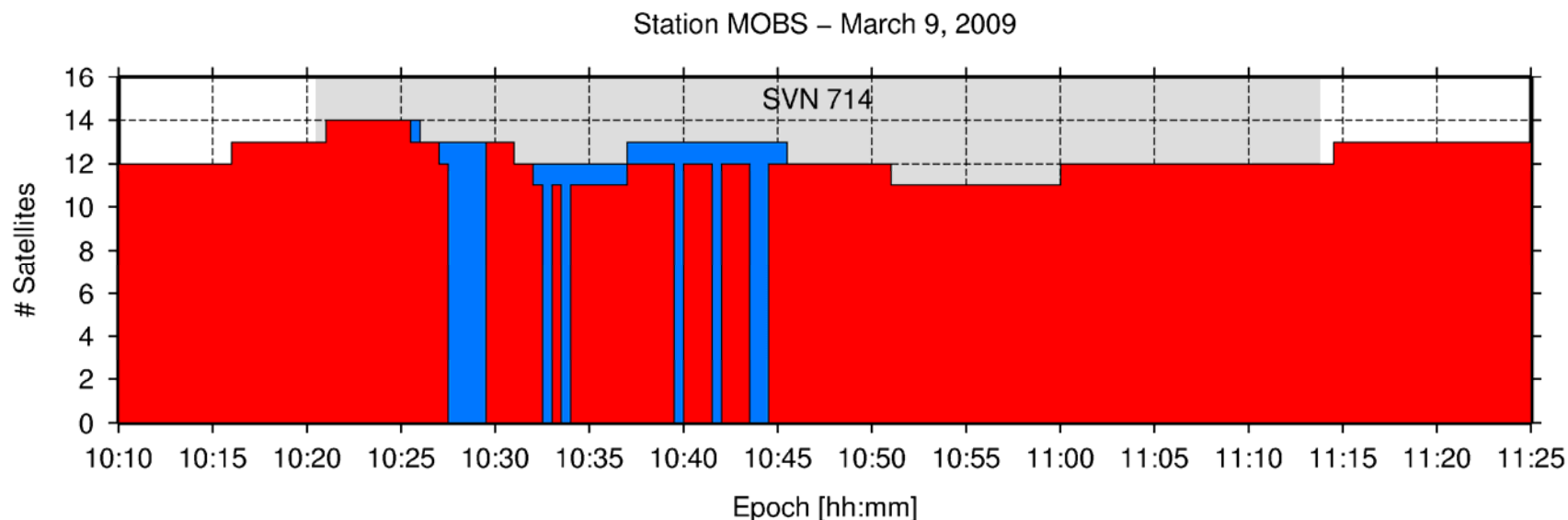
- Nominal attitude model (*red*) vs. new attitude model (*blue*)
- Number of non-rejected ground stations per satellite and epoch
- Drastic decrease in number of stations satisfying outlier test criteria (*red*)
- Significant loss of precision; clock solution even failed in some cases



- Nominal attitude model (*red*) vs. new attitude model (*blue*)
- Degradation of the positioning accuracy of up to a few decimetres (*red*)
- Number of satellites may drop below required minimum  $\Rightarrow$  solution fails
- Problems do not arise when attitude is properly modelled (*blue*)

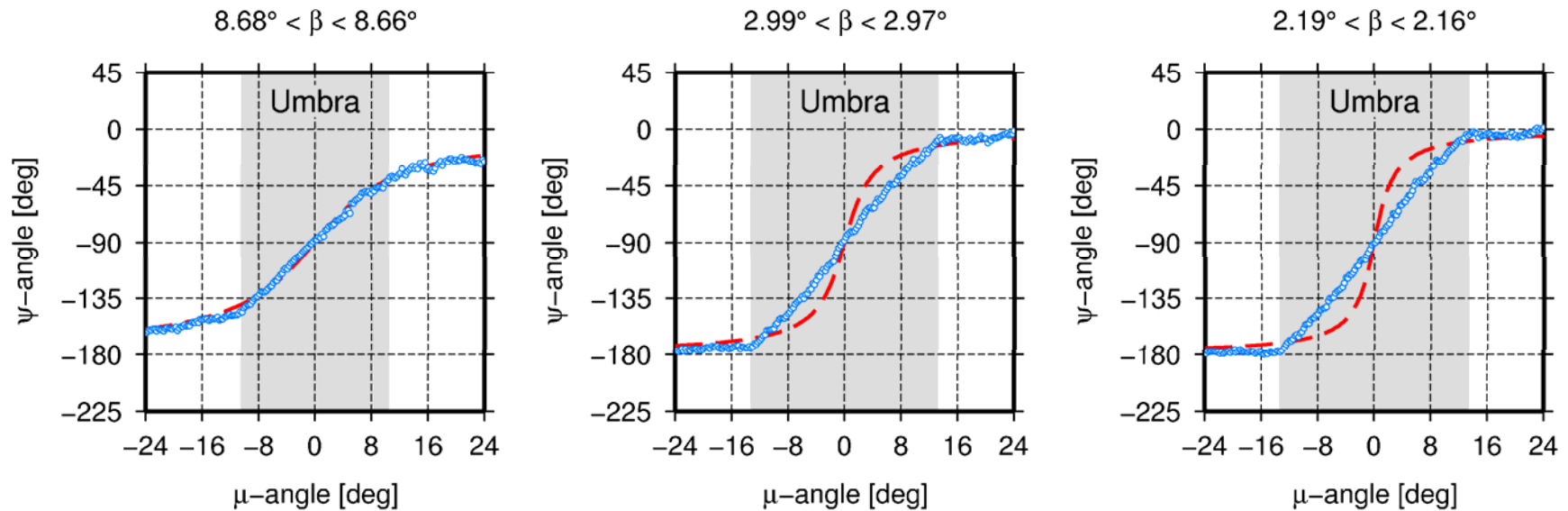


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- Existence of horizontal satellite antenna phase centre eccentricity can be exploited to derive spacecraft's yaw-attitude
- Method has been successfully applied to study yaw-attitude behaviour of eclipsing GLONASS-M satellites
- Nominal yaw-attitude model during eclipse seasons causes range errors on decimetre-level due to mismodelling of satellite APC correction
- Shadow-crossing and noon-turn manoeuvre can be accurately modelled by using a constant yaw rate of  $0.25^\circ/\text{s}$
- Model should also help to improve SLR tracking during eclipse as the centre of the GLONASS-M LRA also exhibits significant horizontal PCO



- S/c tries to keep nominal attitude in Earth's shadow like Block IIRs
- Low yaw rate; slope of straight line fits yields  $0.06^\circ/\text{s}$
- Midnight-turn manoeuvre must be taken into account for  $|\beta| < 7.9^\circ$
- Noon-turn manoeuvre still needs to be investigated